

*RoboSoft 1<sup>st</sup> Plenary Meeting*  
*Pisa*  
*March 31 – April 1, 2014*

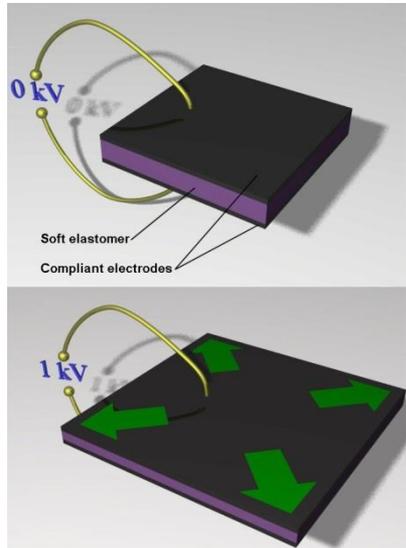
**Optimal energy-harvesting cycles for  
load-driven soft dielectric generators**

*E. Bortot\**, *R. Springhetti\**, *G. deBotton\*\**, ***Massimiliano Gei\****

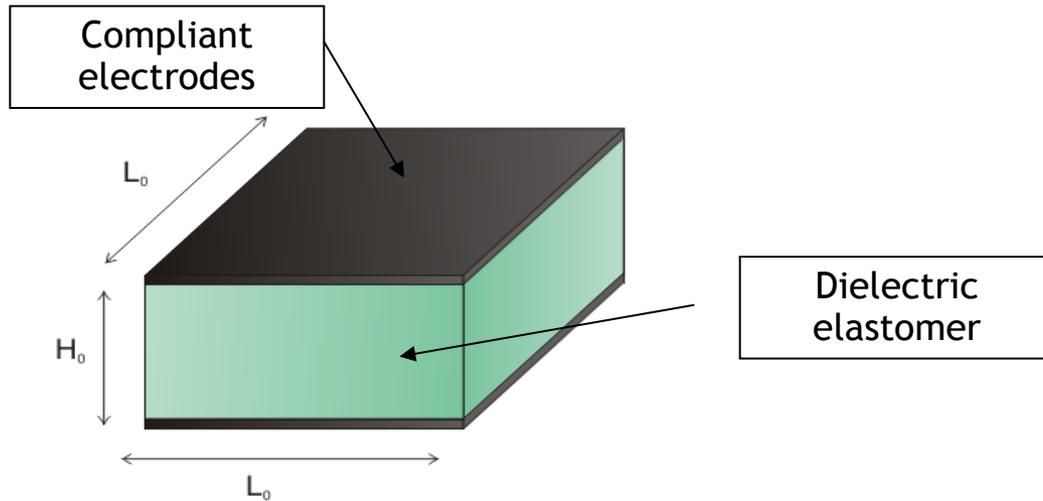
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# DIELECTRIC ELASTOMERS AS ELECTROMECHANICAL TRANSDUCERS



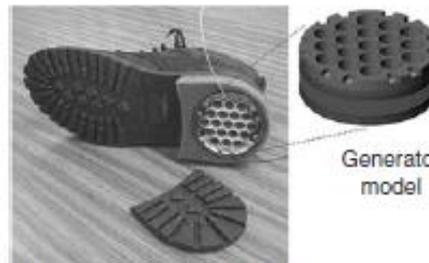
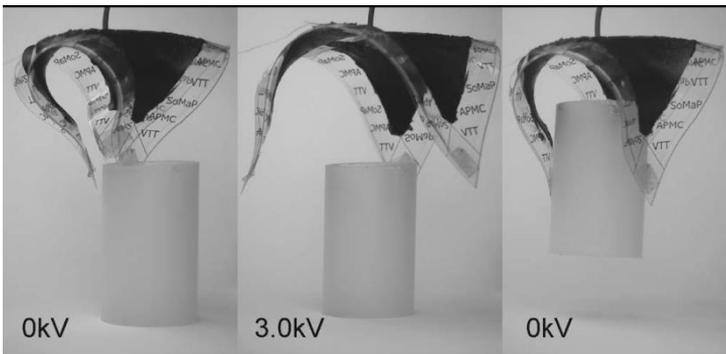
Pelrine et al., Science, 2000



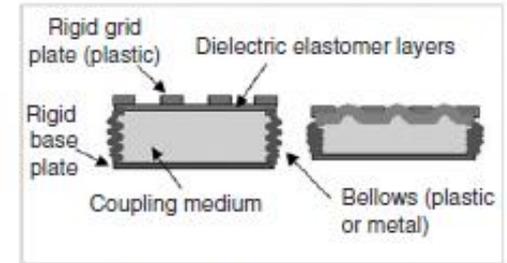
## TRANSDUCER

ACTUATOR

GENERATOR



Mockup of generator installed in boot



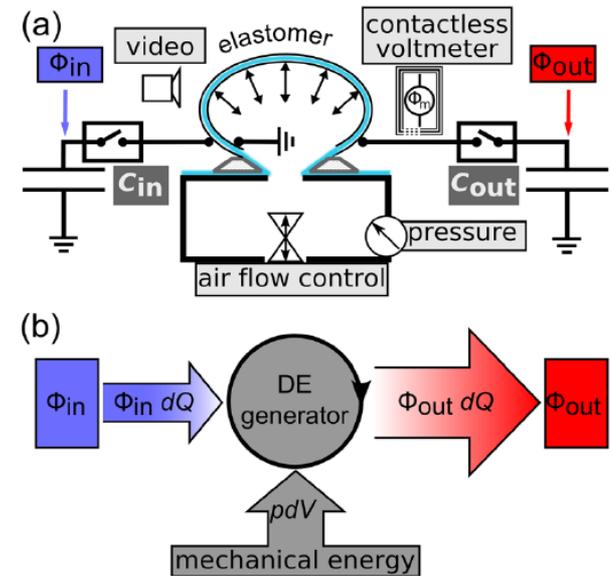
Schematic of generator operation

# MOTIVATION – DEGs AS EMERGING TECHNOLOGY

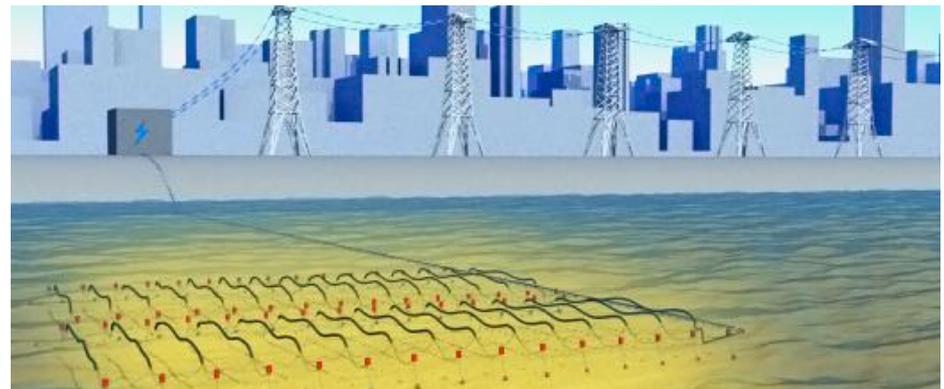
- Research activity on soft homogeneous dielectric elastomer generator (DEG) started around 2007/08 (both theoretically and experimentally).

Relevant papers: Koh et al. (2009), Mc Kay et al. (2011), Foo et al. (2012), Appl. Phys. Lett.

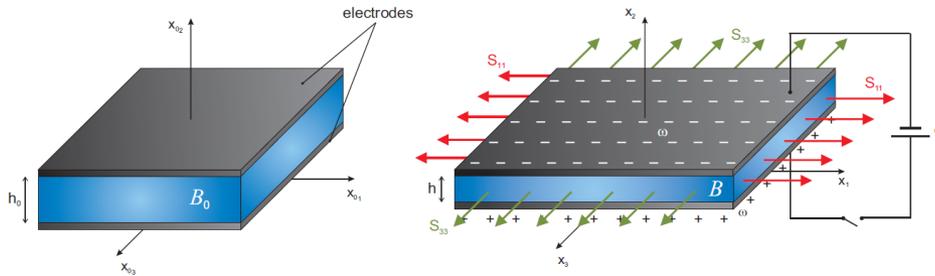
- A large scale project just started in France for exploiting sea-wave motion (by SBM Offshore that designed a large soft DE ring generators of 800mm diameter with multiple layers).



Kaltseis et al. (2012) APL



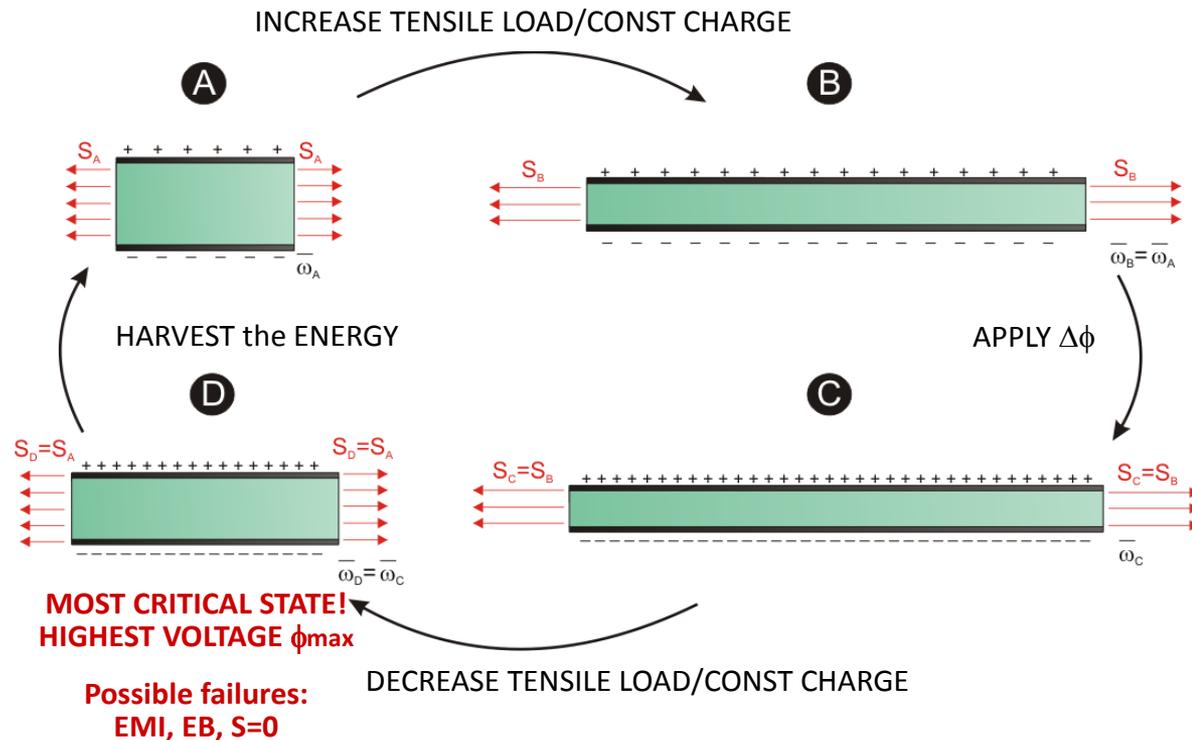
# LOAD-DRIVEN DE GENERATORS: THE MODEL



Soft dielectric generator :  
 homogeneous;  
 neo-hookean;  
 ideal dielectric;  
 subjected to a plane strain state.

Four step load-driven cycle :

1. AB stretch of the layer by increasing the tensile load, constant charge;
2. BC increase in the charge by applying a voltage  $\Delta\phi$ , constant load;
3. CD release the stretch by decreasing the tensile load: the voltage between the electrodes increase;
4. DA harvest the electrical energy by removing the charge surplus at constant load.

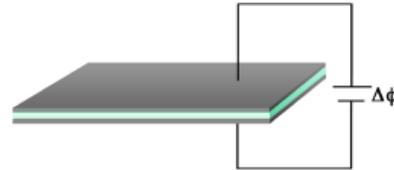


# MODES OF FAILURE

DIELECTRIC ELASTOMERS are susceptible of **SEVERAL MODES OF FAILURE**:

- ELECTROMECHANICAL INSTABILITY

(EMI)



- LOSS OF THE TENSILE STRESS STATE

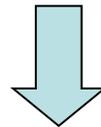
( $\mathbf{S}=\mathbf{0}$ )

- ELECTRIC BREAKDOWN

(EB)

- MATERIAL RUPTURE

( $\lambda_u$ )



**ADMISSIBLE STATE REGION** for the generator

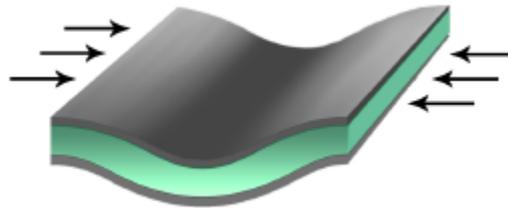
= MAXIMAL ENERGY achievable during a cycle on the ELECTRICAL PLANE

= MAXIMAL ENERGY achievable during a cycle on the MECHANICAL PLANE

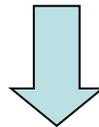
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- ELECTRIC BREAKDOWN (EB)
- MATERIAL RUPTURE ( $\lambda_u$ )



**ADMISSIBLE STATE REGION** for the generator

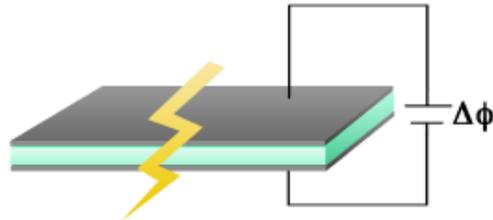
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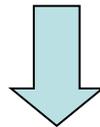
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- MATERIAL RUPTURE

( $\lambda_u$ )



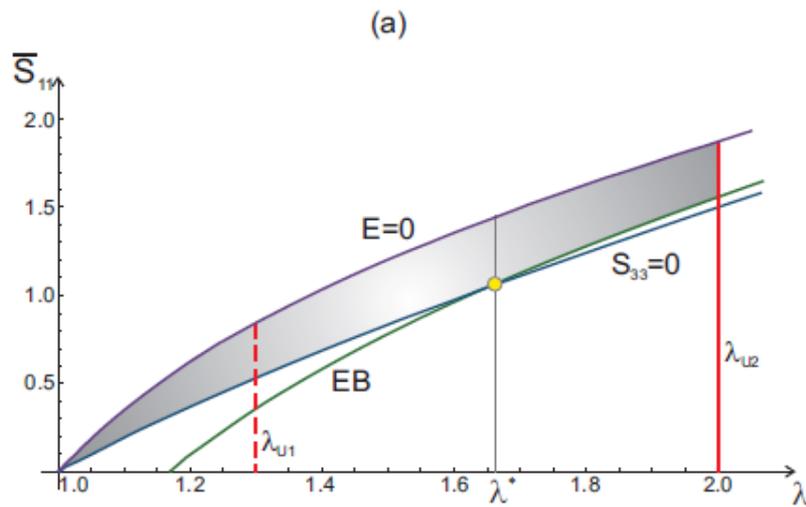
**ADMISSIBLE STATE REGION** for the generator

= MAXIMAL ENERGY achievable during a cycle on the ELECTRICAL PLANE

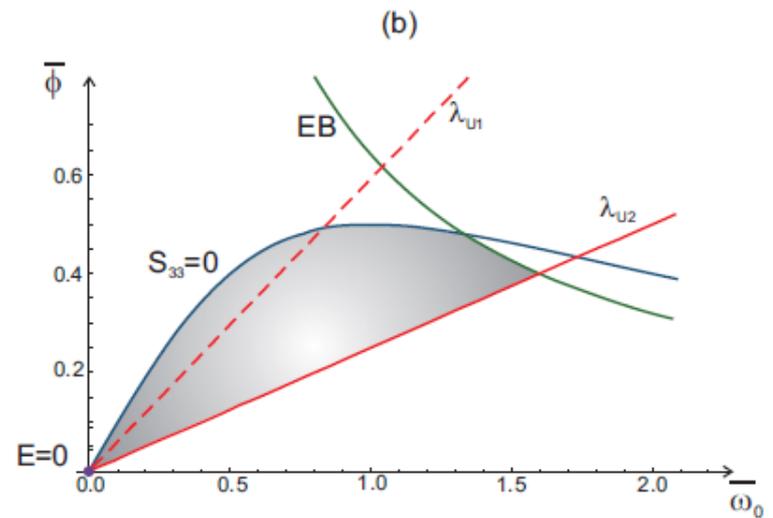
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# ADMISSIBLE STATES REGION

## DIMENSIONLESS QUANTITIES

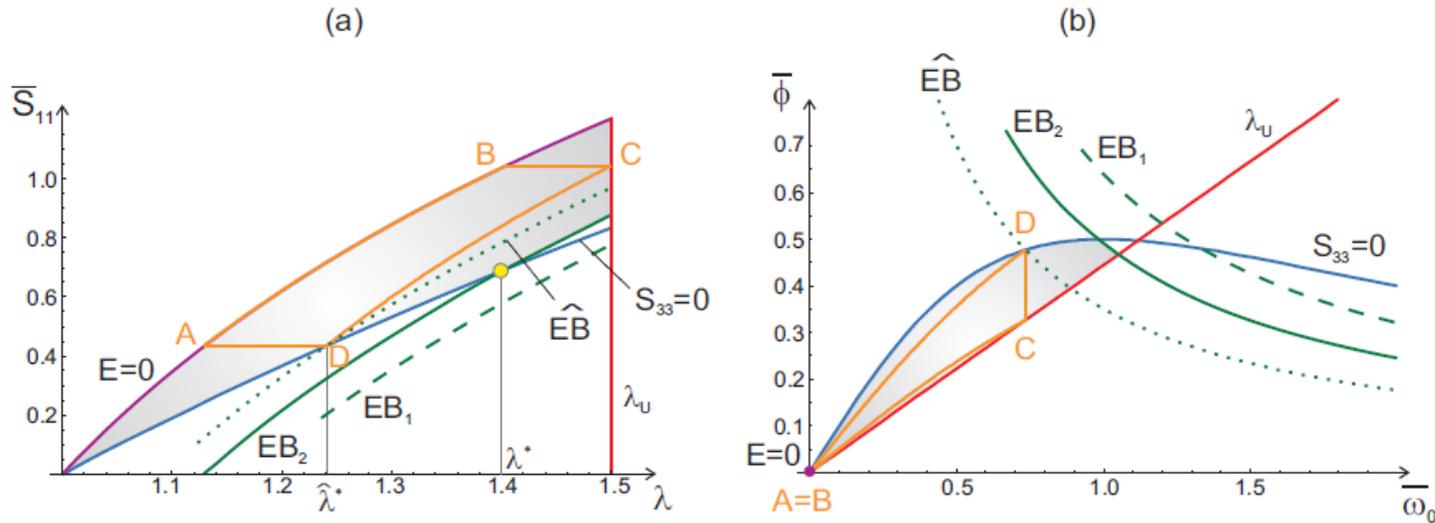


Mechanical plane

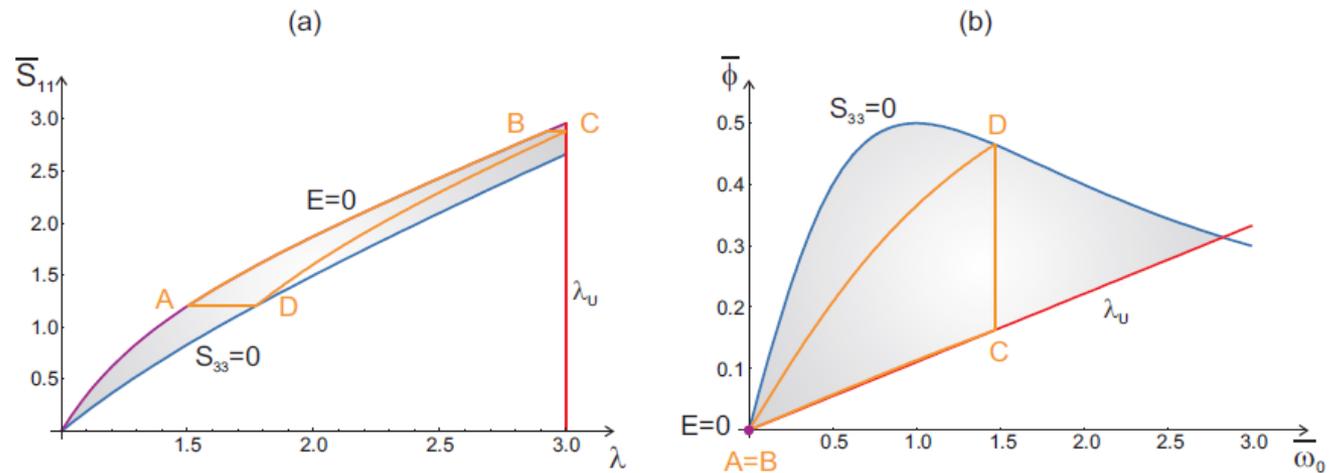


Electrical plane

# OPTIMAL CYCLES FOR DIFFERENT $\lambda_u$



Optimal cycle for  $\lambda_u = 1.5$  with  $E_{eb} \geq 0.5922$ . The dotted curve EB corresponds to the transition between Cases 2a and 2b



Optimal cycle for  $\lambda_u = 3$  with  $E_{eb} \geq 0.5922$

# CONSTRAINED OPTIMIZATION PROBLEM

Expression for the dimensionless generated energy (energy density per unit shear modulus)

$$H_g = \frac{1}{2}(\lambda_A - \lambda_D) [\lambda_D (3\bar{\phi}_D^2 - 1) + 2\lambda_A + 3\lambda_D^{-3}] \\ + \frac{1}{2}(\lambda_C - \lambda_B) [\lambda_B (3\bar{\phi}_B^2 - 1) + 2\lambda_C + 3\lambda_B^{-3}]$$

The optimization problem is formulated as follows

$$\text{find } \min_{\Lambda} H_g[\lambda_A, \lambda_B, \lambda_C, \lambda_D] \quad \Lambda = [\lambda_A, \lambda_B, \lambda_C, \lambda_D]^T$$

subjected to be active constraint  $f[\lambda_A, \lambda_B, \lambda_C, \lambda_D] = -\lambda_C + \lambda_U = 0$ ;

and to the possible active constraints

$$h_1[\lambda_A, \lambda_B, \lambda_C, \lambda_D] = S_{33}^D[\lambda_A, \lambda_B, \lambda_C, \lambda_D] \geq 0,$$

$$h_2[\lambda_A, \lambda_B, \lambda_C, \lambda_D] = -\bar{E}_D^2[\lambda_A, \lambda_B, \lambda_C, \lambda_D] + \bar{E}_{eb}^2 \geq 0,$$

$$h_3[\lambda_A, \lambda_B, \lambda_C, \lambda_D] = \bar{\phi}_B^2 \geq 0 \quad \text{i.e. } \bar{\phi}_B \in \mathbb{R},$$

$$h_4[\lambda_A, \lambda_B, \lambda_C, \lambda_D] = \lambda_A - 1 \geq 0,$$

$$h_5[\lambda_A, \lambda_B, \lambda_C, \lambda_D] = -\lambda_A + \lambda_U \geq 0,$$

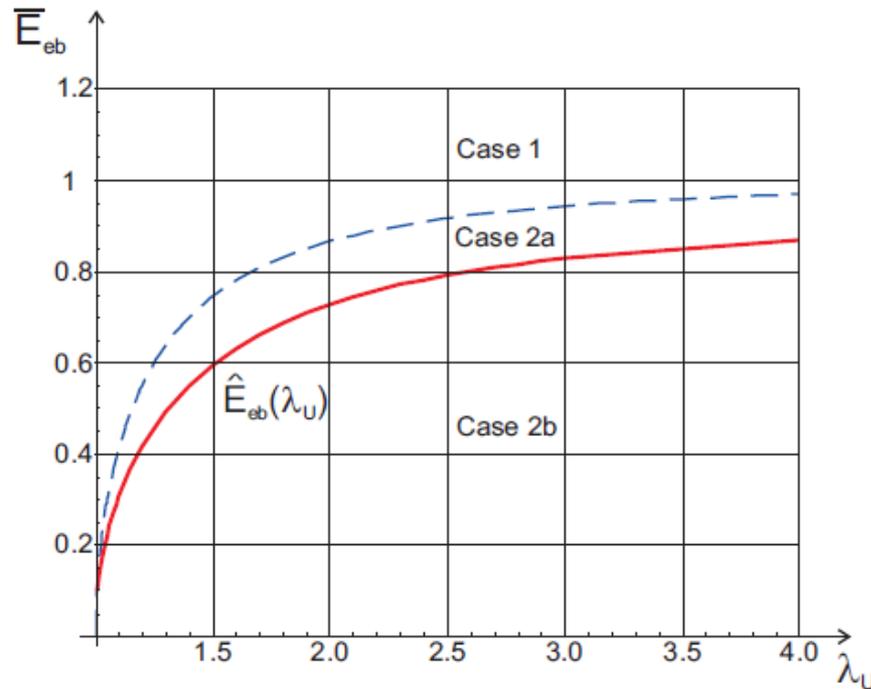
$$h_6[\lambda_A, \lambda_B, \lambda_C, \lambda_D] = \lambda_B - 1 \geq 0,$$

$$h_7[\lambda_A, \lambda_B, \lambda_C, \lambda_D] = -\lambda_B + \lambda_U \geq 0,$$

$$h_8[\lambda_A, \lambda_B, \lambda_C, \lambda_D] = \lambda_D - 1 \geq 0,$$

$$h_9[\lambda_A, \lambda_B, \lambda_C, \lambda_D] = -\lambda_D + \lambda_U \geq 0.$$

# UNIVERSAL CURVE TO EXPLOIT THE FULL POTENTIAL OF A DE MATERIAL



The red curve is an “universal curve” showing the ideal combination of material parameters  $E_{eb} - \lambda_U$  for which the maximum energy can be extracted. If the property pair  $(\lambda_U, E_{eb})$  is located above this curve the optimal cycle will not depend on  $E_{eb}$  and the full potential is not exploited. Thus, in order to extract the maximum from a DEG it is recommended that the pair  $(\lambda_U, E_{eb})$  be as close as possible to the curve.

# GENERATED ENERGY FOR TWO MATERIALS

## 3M VHB-4910 and acrylonitrile butadiene rubber (NBR)

Material	$E_{eb1} = 20 \text{ MV/m}$					$E_{eb2} = 100 \text{ MV/m}$				
	$S_{\max}$ [kPa]	$\mu H_g$ [kJ/m <sup>3</sup> ]	$\Delta\phi/h_0$ [kV/mm]	$\lambda_C$	M-C	$S_{\max}$ [kPa]	$\mu H_g$ [kJ/m <sup>3</sup> ]	$\Delta\phi/h_0$ [kV/mm]	$\lambda_C$	M-C
VHB-4910	94.2	3.99	9.9	1.5	(2b)	87.0	5.33	14.62	1.5	(1)
NBR	94.2	0.37	15.4	1.024	(2a)	87.0	0.32	14.81	1.022	(1)
VHB-4910	246.3	7.60	2.5	3	(2b)	240.5	22.72	7.3	3	(1)
NBR	246.3	1.86	18.2	1.059	(2b)	240.5	2.48	23.3	1.064	(1)



# FURTHER DEVELOPMENTS: VISCOELASTIC EFFECTS

